

Explicit Parameterizations of a Complementary Family of Non-Bending Surfaces

Vladimir Pulov¹ and Ivailo Mladenov²

¹Department of Physics, Technical University of Varna

²Institute of Biophysics, Bulgarian Academy of Science

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Thin-Walled Shells of Revolution

- Shell Element

- Middle Surface of the Shell

- Membrane Theory of Shells

Non-Bending Shells of Revolution

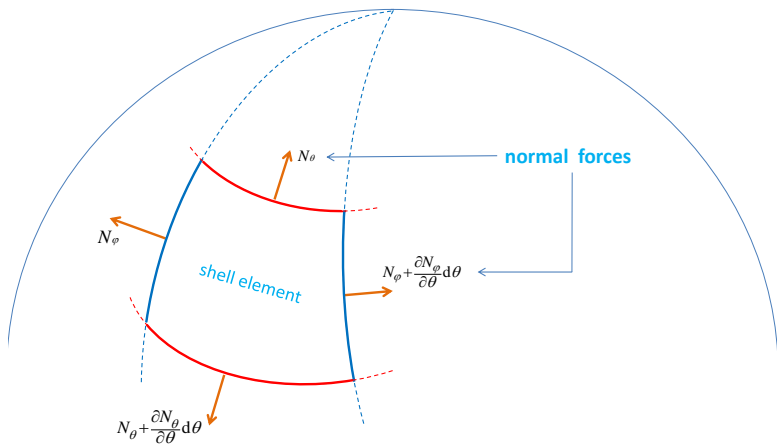
- Non-Bending Condition

- Stress Disturbances at a Fixed Parallel Circle

- Explicit Parameterizations

Possible Applications

Shell Element is cut out by two meridians and two parallels
shearing and transverse forces are neglected



Non-Bending Condition (Gurevich and Kalinin, 1981)

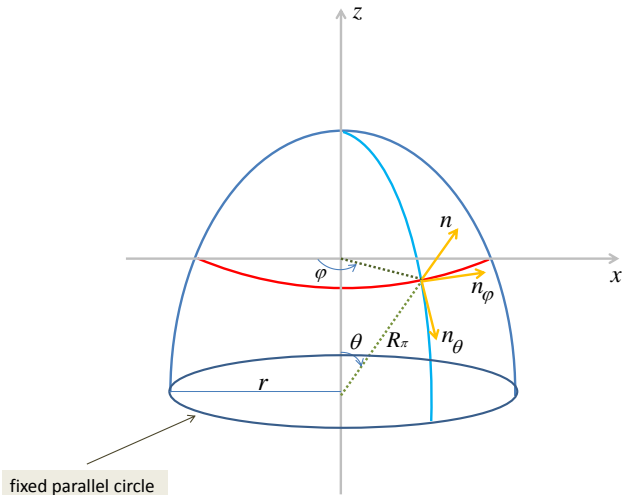
normals do not turn = shell deforms without bending

$$\frac{\kappa_\mu}{\kappa_\pi} \cdot \frac{d}{d\theta} (N_\phi - \nu N_\theta) + (1 + \nu)(N_\phi - N_\theta) \cot \theta = 0$$

κ_μ, κ_π – principal curvatures

N_ϕ, N_θ – normal (direct) forces

Middle Surface of a Shell of Revolution



Stress Equilibrium at a Fixed Parallel Circle (Gurevich and Kalinin, 1981)

$$\dot{N}_\theta = \frac{p}{2\dot{\kappa}_\pi}, \quad \dot{N}_\phi = \frac{p}{2\dot{\kappa}_\pi} \left(2 - \frac{\dot{\kappa}_\mu}{\dot{\kappa}_\pi} \right)$$

p – load

two parametric family of surfaces

represented via elliptic integral

Non-Bending Condition

in terms of principal curvatures κ_π, κ_μ
(Pulov and Mladenov, 2019)

$$\kappa_\mu = 2a\kappa_\pi^2 + 3\kappa_\pi, \quad a = \frac{(\nu - 3)r}{2}$$

four classes of non-bending surfaces

in explicit canonical representations

r, ν – two parameters, $\nu = \frac{\dot{\kappa}_\mu}{\dot{\kappa}_\pi}$

Stress Disturbances at a Fixed Parallel Circle (Gurevich, 1983)

$$\dot{N}_\theta = \frac{p}{2\dot{\kappa}_\pi} (1 + \varepsilon), \quad \dot{N}_\phi = \frac{p}{2\dot{\kappa}_\pi} \left(2 - \frac{\dot{\kappa}_\mu}{\dot{\kappa}_\pi} \right)$$

ε – stress disturbance (perturbation)

Non-Bending Condition ($\varepsilon \neq 0$)

$$\kappa_{\mu} = 2a\kappa_{\pi}^2 + \left(\frac{4a}{r} + \frac{\nu + 3}{\nu - 1}\right)\kappa_{\pi} + \frac{2a}{r^2}, \quad a = \frac{(\nu + 1)(\nu - 3)r}{8(\nu - 1)}$$

two parametric family of non-bending surfaces

r, ν – two real parameters, $\nu = \frac{\dot{\kappa}_{\mu}}{\dot{\kappa}_{\pi}}$

$\varepsilon = \frac{\nu - 3}{\nu - 1}r$ – stress disturbance

Complimentary Family of Non-Bending Surfaces
in the presence of stress disturbances at a fixed parallel circle

$$\kappa_{\mu} = 2a\kappa_{\pi}^2 + \left(\frac{4a}{r} + \frac{\nu + 3}{\nu - 1}\right)\kappa_{\pi} + \frac{2a}{r^2}, \quad a = \frac{(\nu + 1)(\nu - 3)r}{8(\nu - 1)}$$

$\nu = -1, \quad \kappa_{\mu} = -\kappa_{\pi}$ catenoid

$\nu = 0, \quad \kappa_{\mu} = 0, \quad \kappa_{\pi} = \frac{1}{r}$ right circular cylinder

$\nu = 1, \quad \kappa_{\mu} = \kappa_{\pi} = \frac{1}{r}$ sphere

$\nu = 3, \quad \kappa_{\mu} = 3\kappa_{\pi}$ linear Weingarten surface $LW(2)$

Non-Bending Shells of Revolution

Profile of the Middle Surface

Upper Right Branch

$$z(x) = \pm \frac{r}{2} \int_{(x/r)^2}^1 \frac{((\nu + 1)t - \nu + 3)dt}{\sqrt{(1-t)((\nu + 1)^2 t^2 - 2(\nu^2 - 6\nu + 1)t + (\nu + 1)^2)}}$$

plus sign – surfaces inside the cylinder $\nu = 0$ (for $\nu > 0$)

minus sign – surfaces outside the cylinder $\nu = 0$ (for $\nu < 0$, $\nu \neq -1$)

r – radius of a fixed parallel circle

ν – free parameter

Non-Bending Shells of Revolution

Profile of the Middle Surface

Polynomial Under the Radical

$$P(t) = (\nu + 1)^2 t^2 - 2(\nu^2 - 6\nu + 1)t + (\nu + 1)^2$$

Roots

$$\sigma = \frac{1 - 6\nu + \nu^2 + 4(1 - \nu)\sqrt{-\nu}}{(1 + \nu)^2}, \quad \tau = \frac{1 - 6\nu + \nu^2 - 4(1 - \nu)\sqrt{-\nu}}{(1 + \nu)^2}$$

Using Only Elementary Functions

- $\nu = 0$ multiple roots $\sigma = \tau = 1$ (right circular cylinder)
- $\nu = 1$ multiple roots $\sigma = \tau = -1$ (sphere)

Non-Bending Shells of Revolution

Via Elliptic Integrals and Jacobian Elliptic Functions

Open Surfaces Outside the Cylinder $\nu = 0$
(profile curve, $\nu < 0$, $\nu \neq -1$)

$$\eta(u) = \sqrt{\sigma_1 - 1} \operatorname{cn}(u, k_1), \quad k_1 = \sqrt{\frac{\sigma_1 - 1}{\sigma_1 - \tau_1}}, \quad u \in [-K(k_1), 0]$$

$$z_1(u) = \frac{r}{\sqrt{\sigma_1 - \tau_1}} (\lambda_1 F(\operatorname{am}(u, k_1), k_1) + \mu_1 E(\operatorname{am}(u, k_1), k_1))$$

$$\lambda_1 = \tau + \frac{3 - \nu}{1 + \nu}, \quad \mu_1 = \sigma_1 - \tau_1$$

$$x(u) = r\sqrt{1 + \eta(u)^2}, \quad z(u) = z_1(u) - z_1(-K(k_1))$$

Non-Bending Shells of Revolution

Monge Parameterization Via Elliptic Integrals

Open Surfaces Outside the Cylinder $\nu = 0$
(profile curve, $\nu < 0$, $\nu \neq -1$)

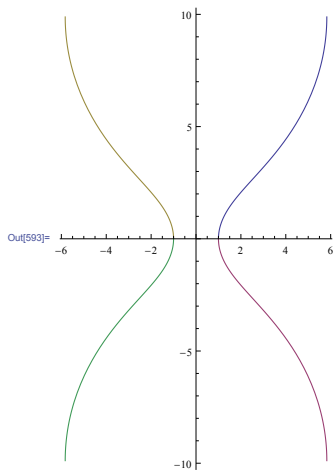
$$z_1(x) = \frac{r}{\sqrt{\sigma_1 - \tau_1}} \left[\lambda_1 F(\varphi(x), k_1) + \mu_1 E(\varphi(x), k_1) - \frac{1}{r} \sqrt{\frac{(\tau_1 - \sigma_1)(x^2 - r^2)(x^2 - \sigma_1 r^2)}{x^2 - \tau_1 r^2}} \right]$$

$$\lambda_1 = \tau + \frac{3 - \nu}{1 + \nu}, \quad \mu_1 = \sigma_1 - \tau_1, \quad k_1 = \sqrt{\frac{\sigma_1 - 1}{\sigma_1 - \tau_1}}$$

$$\varphi(x) = \arcsin \sqrt{\frac{(\sigma_1 - \tau_1)(x^2 - r^2)}{(\sigma_1 - 1)(x^2 - \tau_1 r^2)}}, \quad x \in [r, r\sqrt{\sigma_1}]$$

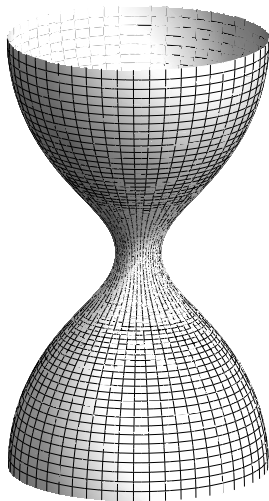
$F(\varphi(x), k_1)$, $E(\varphi(x), k_1)$ – incomplete elliptic integrals

Open Profile Curve ($r = 1$, $\nu = -0.5$)



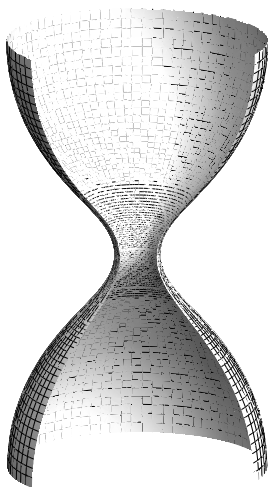
3D View ($r = 1$, $\nu = -0.5$)
Open Non-Bending Surface

Out[99]=



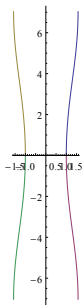
Open Part of 3D View ($r = 1$, $\nu = -0.5$)

Out[111]=

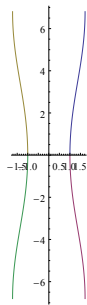


Open Profile Curves

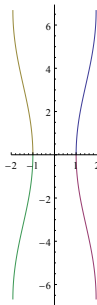
$$\nu = -0.05$$



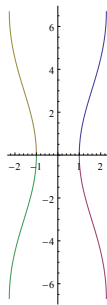
$$-0.07$$



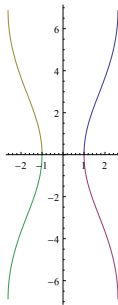
$$-0.1$$



$$-0.15$$



$$-0.2$$



Metal Bellows (Sylphons)

elastic vessels that can be compressed or extended under vacuum

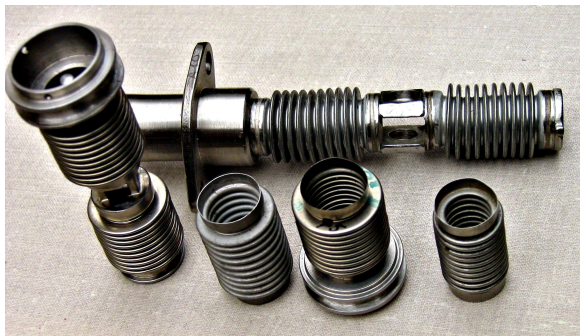
in pressure gauges of aggressive fluids to prevent leakage

in pumps and valves as mechanical seals

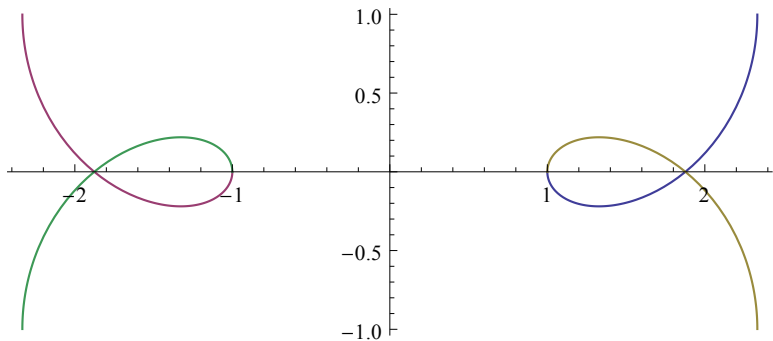
in exhaust gas pipes

compensators of self vibrations and temperature differences

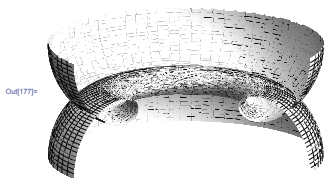
Metal Bellows (Sylphons)



Open Profile Curve ($r = 1$, $\nu = -6.25$)

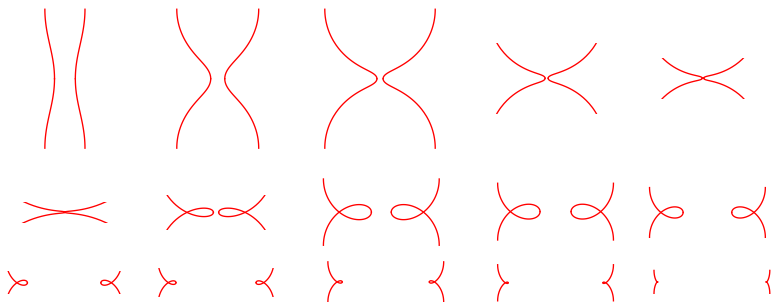


Open Part of 3D View ($r = 1$, $\nu = -6.25$)



Open Profile Curves ($\nu < 0, \nu \neq -1$)

$\nu = -0.1$	- 0.5	- 0.8	- 0.9	- 0.95
-0.99	- 1.2	- 2	- 3	- 10
-20	- 30	- 50	- 100	- 1000



Non-Bending Shells of Revolution

Via Elliptic Integrals

Closed Surfaces Inside the Cylinder $\nu = 0$
(profile curve, $\nu > 0$)

$$z_2(x) = \frac{r}{2\sqrt{A}} \left[\left(\frac{4}{1+\nu} - A \right) F(\varphi(x), k_2) + 2A \left(E(\varphi(x), k_2) - \frac{\sin \varphi(x) \Delta(\varphi(x))}{1 + \cos \varphi(x)} \right) \right]$$

$$A = \frac{1}{2} \sqrt{(\sigma_2 + \tau_2 - 2)^2 - (\sigma_2 - \tau_2)^2}, \quad k_2 = \frac{1}{2} \sqrt{2 - \frac{\sigma_2 + \tau_2 - 2}{A}}$$

$$\varphi(x) = \arccos\left(\frac{A - 1 + (x/r)^2}{A + 1 - (x/r)^2}\right), \quad \Delta(\varphi(x)) = \sqrt{1 - k_2^2 \sin^2 \varphi(x)}, \quad x \in [0, r]$$

$F(\varphi, k_2)$, $E(\varphi, k_2)$ – incomplete elliptic integrals

Closed Profile Curves ($\nu > 0$)

$\nu = 0.01$

1

8



0.1

2

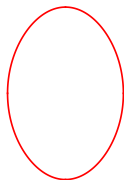
9



0.25

3

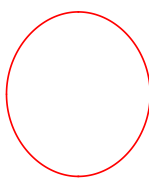
10



0.5

5

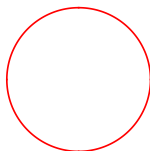
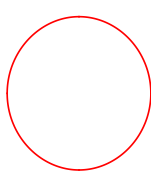
10.5



0.8

7

11



Closed Profile Curves ($\nu > 0$)

$\nu = 11$

12

15

25

50

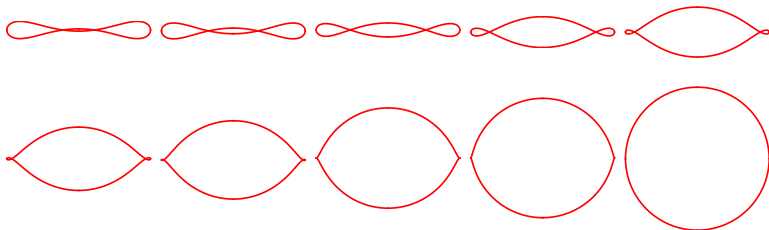
90

200

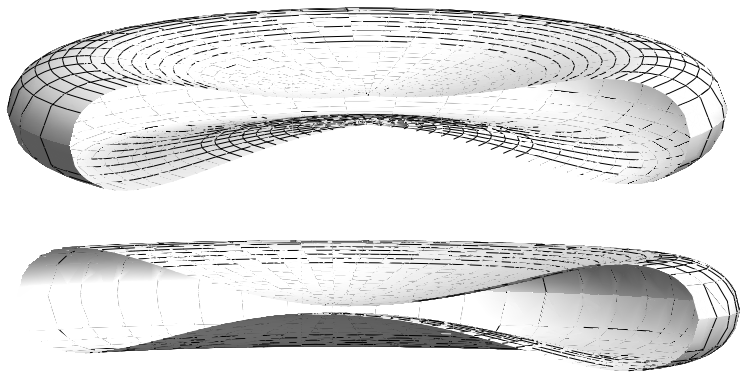
10^3

10^4

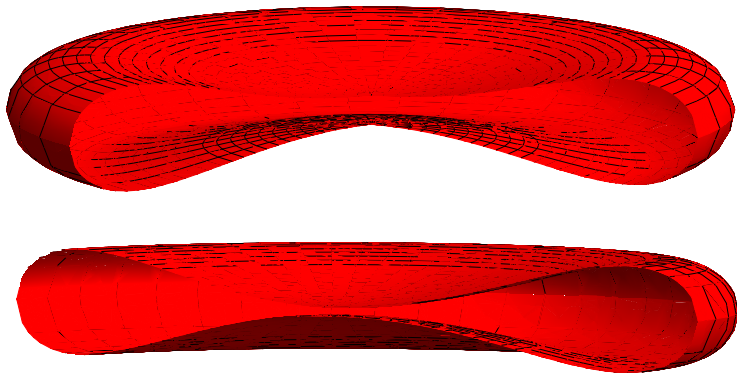
10^{10}



Open Part of 3D View ($r = 1$, $\nu = 9$ and $\nu = 10$)



Open Part of 3D View ($r = 1$, $\nu = 9$ and $\nu = 10$)



Red Blood Cells



References

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